

## **Miniature LED Driver**

#### **PRODUCTION DATA SHEET**

#### DESCRIPTION

The Microsemi LX1995-x is a small inductor and filter capacitor.

The driver supports a wide input start up at 1.6V input. The LX1995-x (switching current is 325mA). driver. The design is based on a (switching current is 500mA). pseudo-hysteretic pulse frequency modulation topology. In portable battery applications the LX1995-x offers high system efficiency with low quiescent current: in operation I<sub>0</sub> is <  $70\mu$ A and in standby I<sub>0</sub> is <  $1\mu$ A.

325mA

500mA

The LX1995-x output current is miniature LED driver with integrated programmable using an external current drivers. It is designed to drive white sense resistor in series with LEDs. This or color LEDs in portable display configuration provides a feedback to the applications. The LX1995-x is an FB pin which maintains constant output adjustable step-up boost converter. current independent of input voltage The LX1995-x can switch up to 2MHz and LED forward voltage (VF). LED allowing designers to use a low cost, dimming is accomplished using a PWM signal or varying DC voltage methods.

The LX1995-x is available in the 5voltage range (1.6V to 5.5V) with Pin TSOT and SOT-23 package. The efficiency greater than 85% and can LX1995-1 can drive up to 6 LEDs The is a low cost, high efficiency LED LX1995-2 can drive up to 10 LEDs

#### **KEY FEATURES**

- < 1µA Shutdown Current</p>
- > 85% Maximum Efficiency
- Efficient at Low Current Levels
- < 70µA Quiescent Supply Current in Operating Mode
- V<sub>IN</sub> Range 1.6V to 5.5V
- Logic Controlled Shutdown
- Dimming Options: PWM or Varying DC Voltage
- Tiny 5-Pin TSOT Package Smallest External Components

#### APPLICATIONS

- Pagers
- Wireless Phones
- PDAs
- LED Driver

LX1995-1CSE

LX1995-2CSE

Digital Camera Displays **GPS** Receivers

IMPORTANT: For the most current data, consult MICROSEMI's website: http://www.microsemi.com



Note: Available in Tane & Reel	Append the letters "TR" to the part number. (i.e. LX1995-1CSG-TR)
	Append the letters first to the part humber. (i.e. Ex1000 1000 11)

-40 to 85 -40 to 85 LX1995-1CSG

LX1995-2CSG



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Supply In	put Voltage	0.3V to 7.0V	0.44	1 5 IN
	Peak Pulse Input Voltage (V <sub>FB</sub> )0.3V		SW	1 5 IN
Shutdowr	n Input Voltage (V <sub>SHDN</sub> )0.3V	V to $V_{IN} + 0.3V$		
	oltage (V <sub>SW</sub> )		GND	2
	urrent (I <sub>SW</sub> )			
	g Temperature Range		FB	
	n Operating Junction Temperature			SG PACKAGE
	emperature Range			(Top View)
Peak Pacl	kage Solder Reflow Temp. (40 second max. exposure)	260°C (+0, -5)		
			SW	1 5 IN
	eeding these ratings could cause damage to the device. All voltages ar and. Currents are positive into, negative out of specified terminal.	e with respect to		
010	and. Currents are positive into, negative out of specified terminal.		GND	2
	THERMAL DATA		FB	3 4 SHDN
SG 1	Plastic TSOT 5-Pin			SE PACKAGE (Top View)
THERM	AL RESISTANCE-JUNCTION TO AMBIENT, $\theta_{JA}$	207°C/W	RoHS / Pb-1	ree 100% Matte Tin Lead Fin
	Plastic SOT-23 5-Pin			
	Plastic SOT-23 5-Pin AL RESISTANCE-JUNCTION TO AMBIENT, $\theta_{1A}$	191°C/W		
THERM	AL RESISTANCE-JUNCTION TO AMBIENT, $\theta_{JA}$	191°C/W		
<b>THERM</b> Junction Te	AL RESISTANCE-JUNCTION TO AMBIENT, $\theta_{JA}$ mperature Calculation: $T_J = T_A + (P_D \ge \theta_{JA})$ .			
<b>THERM</b> Junction Te The $\theta_{JA}$ num	AL RESISTANCE-JUNCTION TO AMBIENT, $\theta_{JA}$			
<b>THERM</b> Junction Te The $\theta_{JA}$ num	AL RESISTANCE-JUNCTION TO AMBIENT, $\theta_{JA}$ mperature Calculation: $T_J = T_A + (P_D \ge \theta_{JA})$ . nbers are guidelines for the thermal performance of the device/pc-boar			
<b>THERM</b> Junction Te The $\theta_{JA}$ num	AL RESISTANCE-JUNCTION TO AMBIENT, $\theta_{JA}$ mperature Calculation: $T_J = T_A + (P_D \ge \theta_{JA})$ . nbers are guidelines for the thermal performance of the device/pc-boar	d system. All of the	N	
<b>THERM</b> Junction Te The $\theta_{JA}$ num	AL RESISTANCE-JUNCTION TO AMBIENT, $\theta_{JA}$ mperature Calculation: $T_J = T_A + (P_D \ge \theta_{JA})$ . nbers are guidelines for the thermal performance of the device/pc-boar ne no ambient airflow. FUNCTIONAL PIN I	d system. All of the	N	
<b>THERM</b> Junction Te The $\theta_{JA}$ num above assur	AL RESISTANCE-JUNCTION TO AMBIENT, $\theta_{JA}$ mperature Calculation: $T_J = T_A + (P_D \ge \theta_{JA})$ . nbers are guidelines for the thermal performance of the device/pc-boar ne no ambient airflow. FUNCTIONAL PIN I	d system. All of the		MOSFET. SW is high
<b>THERM</b> Junction Te The $\theta_{JA}$ num above assur	AL RESISTANCE-JUNCTION TO AMBIENT, $\theta_{JA}$ mperature Calculation: $T_J = T_A + (P_D \ge \theta_{JA})$ . abers are guidelines for the thermal performance of the device/pc-boar ne no ambient airflow. FUNCTIONAL PIN Description Inductor Switching Connection – Internally connected	d system. All of the		MOSFET. SW is high
THERM   Junction Te   The $θ_{JA}$ num   above assur   Name   SW	AL RESISTANCE-JUNCTION TO AMBIENT, $\theta_{JA}$ mperature Calculation: $T_J = T_A + (P_D \ge \theta_{JA})$ . abers are guidelines for the thermal performance of the device/pc-boar ne no ambient airflow. FUNCTIONAL PIN Description Inductor Switching Connection – Internally connected impedance in shutdown.	d system. All of the DESCRIPTION scription	3V N-channel I	
THERM   Junction Te   The $θ_{JA}$ num   above assur   Name   SW   GND	AL RESISTANCE-JUNCTION TO AMBIENT, $\theta_{JA}$ mperature Calculation: $T_J = T_A + (P_D \ge \theta_{JA})$ .   abers are guidelines for the thermal performance of the device/pc-boar   ne no ambient airflow.   FUNCTIONAL PIN I   Des   Inductor Switching Connection – Internally connected impedance in shutdown.   Common terminal for ground reference.   Feedback Input – Connect to a current sense resistor	d system. All of the DESCRIPTIO scription to the drain of a 28	3V N-channel I and GND to se	et the maximum output



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## ELECTRICAL CHARACTERISTICS

Unless otherwise specified, the following specifications apply over the operating ambient<sup>1</sup> temperature  $0^{\circ}C \le T_A \le 70^{\circ}C$  except where otherwise noted and the following test conditions:  $V_{IN} = 3V$ ,  $V_{\overline{SHDN}} = V_{IN}$ . Unless where indicated, these parameters apply to both the LX1995-1 and LX1995-2 part versions.

Parameter	Symbol	Test Conditions	LX1995-x			Units	
Falameter	Symbol	Test conditions	Min	Тур	Max	Units	
Operating Voltage	V <sub>IN</sub>		1.6		5.5	V	
Minimum Start-up Voltage	V <sub>SU</sub>	$T_A = +25^{\circ}C$			1.6	V	
Start-up Voltage Temperature Coefficient	<b>k</b> <sub>VST</sub>	Guaranteed; not tested		-2		mV/°C	
Quiescent Current		Not switching		70	100		
	IQ	$V_{\overline{SHDN}} < 0.4V$		0.2	0.5	μA	
FB Threshold Voltage	V <sub>FB(TH)</sub>		288	320	352	mV	
FB Input Bias Current	I <sub>FB</sub>	Not Switching, V <sub>FB</sub> = 400mV	-10		10	nA	
Shutdown Input Bias Current	I SHDN	$V_{\overline{SHDN}} = 0V$	-100		100	nA	
Shutdown Low Input Voltage	V				0.6	V	
Shutdown High Input Voltage	V <sub>SHDN</sub>		1.4			v	
Switch Peak Current	IPEAK	L= 47µH; LX1995-1	250	325	400	mA	
Switch Peak Current	IPEAK	L= 47µH; LX1995-2	<mark>4</mark> 00	500	600	mA	
Minimum Switch Off-Time	t <sub>OFF</sub>	$T_{A} = +25^{\circ}C; V_{FB} < V_{FB(TH)}$		300		ns	
Switch Pin Leakage Current	ILEAK	$V_{SW} = 28V$		0.23		μΑ	

Note:

1. Low duty cycle pulse testing techniques are used which maintains junction and case temperatures equal to the ambient temperature.

2. Functionality over the -40°C to +85°C operating temperature range is assured by design, characterization, and correlation.



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APPLICATIONS

Microsemi<sub>®</sub>

# LX1995

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#### THEORY OF OPERATION

#### **OPERATING THEORY**

The LX1995-x is a PFM boost converter optimized for driving a series of white or color LEDs. It operates in a pseudo-hysteretic mode with a fixed, 300ns, switch "off time". When the LX1995-x enables, the LED current decreases causing the FB voltage to decrease to a value less than 320mV. The feedback comparator (See Simplified Block Diagram) activates the control logic. The control logic turns on the DRV output circuit that connects to the internal N-Channel MOSFET gate. The switch output (SW) is switched "on" and remains "on" until the inductor current ramps up to the peak current level (typically 325mA for LX1995-1).

The LED load is powered from energy stored in the output capacitor during the inductor charging cycle. Once the peak inductor current value is achieved, the output is turned off and the energy stored in the inductor delivers to the load. This causes the voltage to rise across the current setting resistor ( $R_1$ ) at the input to the feedback circuit. The LX1995-x continues to switch until the voltage at the FB pin exceeds 320mV. The value of  $R_1$  is calculated by dividing 320mV by the maximum series LED current. A minimum value of 3.3 $\Omega$  is recommended for  $R_{SET}$ . The voltage at the FB pin is the product of the LED current ( $I_{LED}$ ) and  $R_1$ .

 $R_1 = \frac{1}{I_{LED(MAX)}}$ 

#### **DIMMING METHODS**

LX1995-x supports two dimming methods: PWM or DC Voltage.

**PWM mode:** Connect system PWM logic signal to the SHDN pin (See Figure 1). This turns the LX1995-X on and off which pulses the LED current between zero and the setting determined by  $R_1$ .

**DC Voltage mode:** The designer can apply an adjustable DC voltage supply to the FB pin. As the DC voltage increases, the LED current decreases. The equation (see Figure 3) is:

$$I_{LED} = \frac{1}{R_1} \left[ 320 \text{mV} \cdot \left( \frac{R_2 + R_3}{R_3} \right) - V_{ADJ} \cdot \left( \frac{R_2}{R_3} \right) \right] \qquad \text{eq. 2}$$

#### INDUCTOR SELECTION AND OUTPUT CURRENT LIMIT PROGRAMMING

Microsemi recommends the use inductors (for the LX1995-1) in the range of  $10\mu$ H to  $47\mu$ H due to saturation of peak inductor current. By increasing the average inductor current, the LX1995-x will extend the power range. Smaller inductor values will reduce output voltage ripple and are smaller in size.

#### **OUTPUT RIPPLE AND CAPACITOR SELECTION**

Output voltage ripple is depended on the selection of the inductor value (L), output capacitor value ( $C_{OUT}$ ), peak switch current ( $I_{PEAK}$ ), load current ( $I_{OUT}$ ), input voltage ( $V_{IN}$ ) and the output voltage ( $V_{OUT}$ ). The peak-to-peak voltage ripple is a function of the output droop (as the inductor current charges to  $I_{PEAK}$ ), the feedback transition error (i.e., typically 10mV), and the output overshoot (energy stored in the inductor). When the switch is first turn on, the total ripple voltage is:

$$V_{\text{RIPPLE}} = \Delta V_{\text{DROOP}} + \Delta V_{\text{OVERSHOOT}} + 10 \text{mV}$$
 eq. 3

The initial droop can be estimated with the assumption of 0.5V of voltage drop across the inductor and FET RDS<sub>ON</sub>.

$$\Delta V_{\text{DROOP}} = \frac{\left(\frac{L}{C_{\text{OUT}}}\right) \cdot \left(I_{\text{PK}} \times I_{\text{LED}}\right)}{V_{\text{IN}} - 0.5} \qquad \text{eq. 4}$$

The output overshoot calculated with 0.5V as voltage drop across the diode.

$$\Delta V_{\text{OVERSHOOT}} = \frac{\frac{1}{2} \cdot \left(\frac{L}{C_{\text{OUT}}}\right) \cdot \left(I_{\text{PK}} - I_{\text{LED}}\right)^2}{V_{\text{OUT}} - V_{\text{IN}} + 0.5} \qquad \text{eq. 5}$$

Once the output voltage ripple is determined for the selected components, the output capacitor can then be adjusted to meet the target ripple voltage requirements.

The LX1995-x is targeted for LED driver applications; output voltage ripple is not a critical application requirement.

eq. 1



## **Miniature LED Driver**

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CHARTS

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Note: Dimensions do not include mold flash or protrusions; these shall not exceed 0.155mm(.006") on any side. Lead dimension shall not include solder coverage.



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NOTES

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